

| Request reference number (to be filled by MHD): (2014)-02-05 Date: 2017-03-24 | | | | | | | |
|---|----------------------------|--------------------|---------|---|--|--|--|
| Please fulfil the | following | | | | | | |
| Part: EN 13445-2 | lssue: 2014 | Page 16 | Sub | clause 5 | National Standard Reference | | |
| Subject: Materials used for non-pressure parts | | | | | | | |
| Type of request: | 🛛 Tech | nical clarificatio | on | | Editorial correction | | |
| | 🗌 Tech | nical comment | | | Translation correction | | |
| From : Company: VSK Pardubice s.r.o. Name: Tereza Bílková Postal address: Stará Obec 312 533 54 Pardubice-Rybitví Czech Republic | | | | e-mail:tereza.bilkova@vsk.cz phone: +420 732 418 194 | | | |
| Manufacturer | User | Other (p | lease s | specify): | | | |
| Question/comment: In subclause 5 it is said, that for non-pressure parts you have to use materials with specified chemical composition and tensile properties. In shell-and-tube heat exchangers baffles are used to provide desired flow pattern and support tubes. Baffles are placed in shell which is working under pressure. But baffles themselves are not subject to any pressure load. Is it possible to use materials mentioned in subclause 5 for baffles? Or is it necessary to use materials corresponding to subclause 4? Proposed answer(s): * As baffles do not transmit any pressure load, materials for non-pressure parts mentioned in subclause 5 can be used. | | | | | | | |
| Answer from the I | WHD (to be filled b | y MHD): | | | | | |
| Agree with the proposed answer. | | | | | | | |
| To be sent to EN 13445 Maintenance Help Desk secretariat: EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr | | | | | HD secretariat c/o UNM ion Office on behalf of AFNOR s La Défense Cedex – France 445@unm.fr | | |



| Request reference number (to be filled by MHD): (2014)-0 | | | | 02-09 | <u>Date</u> : 2019-04-14 | | |
|--|--|------------|-------------------------|-------------------------------|---|--|--|
| Please fulfil the | following | | | | | | |
| Part: EN 13445-2 | lssue: 2009 | Page 51 | Subo Anr | clause nex D | National Standard Reference | | |
| Subject: Technical | Subject: Technical delivery conditions for Clad products for pressure purposes | | | | | | |
| Type of request: | Type of request: Image: Technical clarification Image: Editorial correction Image: Technical comment Image: Translation correction | | | | | | |
| From : Company: Rolls-Royce Name: Shaun Currie Postal address: 303 Bridgewater Place, WA3 6XF. UK | | | UK | e-mail: <u>sl</u> phone: + | naun.currie@rolls-royce.com 44 (0) 1925 781746 | | |
| Anufacturer | User | Other (| Other (please specify): | | | | |



Question/comment:

Dear Sir / Madam, we have a query regarding components that are to be explosive clad, to EN13445-2. The components are both Tubesheets, one in P245 GH Carbon Steel at \emptyset 2.3m x 80mm main section and the other in P265 GH at \emptyset 2.1m x 130mm main section, finished sizes.

Both Tubesheets are to be clad in Titanium to B265, 10mm thick, with a finished thickness of 6mm.

The cladding operation is being completed by an external supplier.

They are working to EN13445-2, Annex D, and our customer, EDF, spec BTS 91.C.109.UKEPR, Appendix 19. The EDF spec states the following 'When the cladding is carried out by explosion, the test specimens shall be taken in the zone furthest away from the ignition point'.

In this instance, the ignition point would therefore be at 180° to the test piece location.

This was originally mutually agreed by a procurement spec.

Since then, the supplier is now asking for a concession on this point.

The supplier is asking the following;

"In order to increase as much as possible the material for test specimens, the Tubeplate to be obtained has been moved on one side of starting forging (180°), leaving 50 mm in order to guarantee the adhesion of titanium plate after cladding on entire surface of Tubeplate.

At the same time the ignition point has been positioned at 270° (previously 180°) of starting forging, in order to increase the distance between ignition point and the Tubeplate, and respect as far as possible the BTS requirements about the placement of test specimens."



RR are looking to determine if this is an acceptable proposal. We would also like to determine the following;

- The effect of having the test pieces positioned furthest away from the ignition point, does this give better or worse case mechanical results?
- What effect (if any) is likely by following our supplier's proposal. Are we likely to see better or worse mechanical results?
- The effect of the test pieces positioned at the edge of the component. Are there any detrimental effects due to the shape of the component, and the location of the test pieces?

Thanks in advance for your help. Kind regards, Shaun

Proposed answer(s): *



Answer from the MHD (to be filled by MHD):

Tis is a specific technical specification to EDF. Informative Annex D of EN 13445-2 has no recommendation on this matter

| To be sent to EN 13445 Maintenance Help Desk secretariat: | EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr |
|---|--|
| | |



| Request reference number (to be filled by MHD): (2021)-03-02 Date: 2022-05-05 | | | | | | |
|---|--|---------------------------|---|-------------|---------------------------------|--|
| Please fulfil the | following | | | | | |
| Part: EN 13445-3 | Issue: 2021 | Page 363 & 374 | e Subclause 374 16.4.6.4 & 16.5.6.4 | | National Standard Reference | |
| <u>Subject</u> : | | | | | | |
| Type of request: | 🗌 Tec | hnical clarifica | ation | | Editorial correction | |
| | 🗌 Те | chnical comm | ent | | Translation correction | |
| From : | | | | | | |
| Company:P3 Engin | eering | | | e-mail:W | V.Stikvoort@P3Engineering.nl | |
| Name:Walther Stik | voort | | | phone: + | -31592347088 | |
| Postal address:Rot | tterdamseweg 183 | SC - 2629 HD I | Delft | | | |
| The Netherlands | | | | | | |
| | | | | ; | Concultors | |
| | | | please | specity): (| Consultant | |
| Question/common | | | | | | |
| Question/commen | <u>nt</u> : | | | | | |
| Re:Clause 16. | 4.6.4 of EN 1 | 3445-3 | anatio | n (16 | 4 15) | |
| Add the foll | owing expressi | | quatio | n (10. | 4-13) | |
| $\int [(\Phi_{\rm P} + \Phi_{\rm Z})]$ | $)^{2} + \Phi_{B}^{2} +$ | $\Phi_{\rm T}^2 \le 1.0$ | | | (16. 4-15a) | |
| N | | | | | | |
| $\sqrt{\Phi_{\pi}^2 + \Phi_{\mu}^2}$ | $+\Phi_{r}^{2} < 1.0$ | | | | (16, 4-15b) | |
| V - Z · - B | 1 = 1.0 | | | | (10) 1200) | |
| $\sqrt{(\Phi_{\rm P} - 0.2)}$ | $ \Phi_{\rm Z})^2 + \Phi_{\rm B} ^2$ | $+\Phi_{s}^{2} \leq 1$ | .0 | | (16. 4-15c) | |
| | | | | | | |
| Re:Clause | 16.5.6.4 of EN | 13445-3 | | | 15 | |
| Add the foll | owing expression | ions under e | quatio | n (16. 5 | -15) | |
| $\left[\left(\left \frac{\Phi_{P}}{2}+\Phi_{Z}\right \right]\right]$ | $)^{2} + \Phi_{B}]^{2} +$ | $-\Phi_{\rm T}^2 \le 1.0$ | | | (16. 5-15a) | |
| N 64 | | | | | | |
| $\sqrt{\Phi_n^2 + \Phi_n^2}$ | $+\Phi_{m}^{2} < 1.0$ | | | | (16, 5-15b) | |
| V 12 1 1B | 1 1 2 1.0 | | | | (10. 5 155) | |
| $\sqrt{\left(\left \frac{\Phi_P}{c_4}\right - 0.2\right)}$ | $ \Phi_{\rm Z})^2 + \Phi_{\rm B}^2$ | $+\Phi_{s}^{2} \leq 1$ | .0 | | (16. 5-15c) | |
| | | | | | | |
| Proposed answer(s | <u>s)</u> : * | | | | | |
| Desired addition to | clarity the correct | Interpretation | i of the (| equations | (16.4-15) and (16.5-15) | |



Answer from the MHD (to be filled by MHD):

We think that the formulae contained in the standard are clear enough. The proposed answer is not acceptable.

| To be sent to EN 13445 Maintenance Help Desk | EN 13445 MHD secretariat c/o UNM |
|--|--|
| secretariat: | Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr |

| Request reference number (to be filled by MHD): (2014)-03-61 Date: 2021-07-26 | | | | | | | |
|---|------------------|---|-------------------------|---|---|--|--|
| Please fulfil the | following | | | | | | |
| Part: EN 13445-3 | lssue: 2014 | Page 28 | Subclause 6.6.2 | | National Standard Reference | | |
| Subject: | | | | | | | |
| Type of request: | 🔀 Tech | nical clarificati | on | | Editorial correction | | |
| | 🗌 Tech | nical comment | t | | Translation correction | | |
| From : Company: Milton Roy Europe Name: Bringuier Jean-Baptiste Postal address:10 Grande Rue, 27360 Pont-Saint-Pierre | | e-mail: Jean-Baptiste.Bringuier@miltonroy.com phone: +33 7 61 30 99 83 | | | | | |
| Manufacturer | User | Other (| please s | specify): | | | |
| Question/comment: For the static and fatigue sizing of a machined part, the EN13445-3 considers austenitic and ferritic steels only, what about austenitic-ferritic steels like duplex and superduplex? What calculation method should we use? | | | | | | | |
| Part cut in 4 Proposed answer(s): * In fatigue, use the calculation method for ferritic steels and in static, use the first line of table 6-1 because it is the most restrictive equations for steels other than austenitic. Answer from the MHD (to be filled by MHD): | | | | | | | |
| The proposed answ | ver is accepted. | | | | | | |
| To be sent to EN 1 secretariat: | 3445 Maintenand | e Help Desk | EN Sta F 9 e-r | 13445 M andardizat 2038 Pari nail: <u>en13</u> | HD secretariat c/o UNM ion Office on behalf of AFNOR is La Défense Cedex – France 445@unm.fr | | |



| Request reference number (to be filled by MHD): (2014)-03-62 Date: | | | | | | | |
|---|--|-----------------------------------|-------------------------------|---------------------------|--------------------------------------|----------------------------|-------------|
| Please fulfil the following | | | | | | | |
| Part: EN 13445-3/A | Issue: A8 2019 | Page 12 & 22 | Sub 16. &16 | clause 4.5.7 .5.5.7 | Nati | onal Standard Referenc | ce |
| <u>Subject</u> : | | | | | | | |
| Type of reques | st: 🗌 Tech | nical clarificati | on | | Editorial corre | ection | |
| | 🗌 Tech | inical commen | t | | Translation c | orrection | |
| From : | | | | | | _ | |
| Company:N.A | | | | e-mail:st | ikvoort@zigg | o.nl | |
| Name:Walther | Stikvoort | | | phone: + | 3159234708 | 8 | |
| Postal address: | Wagnerlaan 37; 9402 | SH Assen (NL | .) | | | | |
| | | | | | | | |
| Manufacture | er 🗌 User | Other (| please s | specify): C | Consultant Sta | atic Pressure Equipmen | t Integrity |
| | | | | | | | |
| Question/com | ment: | | | | | | |
| | | | | | | | |
| The formulas formulas for mean nozzle di | r determining the she ameter in order to be | ar stresses sh consistent with | ould be h WRC [/] | based on 107 and P | the outside i D 5500 claus | nozzle diameter rather t | han the |
| | | | | | | | |
| PDC | | | | | | | |
| | I | | | | | | |
| OCAL_STRESS_ST | _L ATI | | | | | | |
| | | | | | | | |
| The pdf shows | shear stress formulas | based on out | side diar | neter (rad | lius) of the no | zzle! | |
| Plaasa includa | this in the 2021 editio | n of EN 13115 | 2 hv m | oons of or | addondum | | |
| Flease include | | II 0I EIN 13443 | -3 by m | | | | |
| Proposed answ | <u>er(s)</u> : * | | | | | | |
| Proposed adap | tation of shear stres | <u>s formulae</u> | | TNI 19445 | 2 | | |
| Re: EN 13445 | 3:2014 / A8 : 2019 an | a the 2021 ver | sion of I | EN 13445 | -3 | | |
| The mean nozz | le diameter "d" will b | e replaced by t | he outsi | de nozzle | diameter "de' | ' in the equations for the | e shear |
| stresses as state | d in clauses: 16.4.5.7 | ,16.4.7.3,16.5.: | 5.7 and | 16.5.7.3 to | be consisten | nt with WRC Bulletin 10 | 07. |
| | | | | | | | |
| The relevant cla | auses in combination | with the releva | nt equat | 10 are s | ummarized ir | the table below: | |
| Equations | 10.4.3.7 | 10.4.7.3 | | 10.5.5. | 2): | (16.5.7.5) | |
| Equations | (10.4-8a), $(16.4-8b)$ | (10.4-22a); $(16.4-22b)$ | | (16.5-8) | a), b): | (16.5-24b); | |
| | (10.1.00) | (10.1 220) | | (16.5-8 | Bc) | (16.5-24c) | |
| Answer from t | he MHD (to be filled b | | | | | | |
| Answer Holli (| | <i>y</i> wii <i>D</i>). | | | | | |
| The method of EN 13445.3 is an original method, there is no need to modify it considering methods provided by other standards. The proposed modification is not accepted. | | | | | | | |



| To be sent to EN 13445 Maintenance Help Desk | EN 13445 MHD secretariat c/o UNM |
|--|---|
| secretariat: | Standardization Office on behalf of AFNOR |
| | F 92038 Paris La Défense Cedex – France |
| | e-mail: <u>en13445@unm.fr</u> |
| | |



| Request reference number (to be filled by MHD): (2014)-03-63 Date: 201X-xx-xx | | | | | | | | |
|--|--------------------|--|-------------------------|--|---|--|--|--|
| Please fulfil the | following | | | | | | | |
| Part: EN 13445-3 V4 | lssue: 2014 | Page 162 | Sub | clause 11 | National Standard Reference French | | | |
| <u>Subject</u> : | Subject: | | | | | | | |
| Type of request: | 🛛 Tech | nical clarificatio | on | | Editorial correction | | | |
| | 🗌 Tech | nical comment | i | | Translation correction | | | |
| <u>From</u> : Company: Cetim Name: Philippe ROHART Postal address: Avenue Felix Louat, Senlis, FRANCE | | e-mail: philippe.rohart@cetim.fr phone: +33 3 44 67 47 94 | | | | | | |
| Manufacturer | 🛛 User | Other (| olease | specify): | | | | |
| Question/comment: Clause 11.5.1 provides a set of information about flange calculations. Clause 11.5.1.b provides a methodogy, whose applicability depends on some parameters. One of them requires that P should be lower or equal to 2 MPa. Question : In this equation, what is P ? Proposed answer(s): * Proposed answer 1 : P is unique for a flange, and is the highest pressure value applied on the flange. It should be the test pressure. Proposed answer 2 : P is the pressure for the situation evaluated. Therefore, if a flange is calculated for a service situation and a test situation, the service situation may be evaluated with clause 11.5.1.b if the pressure is lower or equal to 2 MPa, while the test situation would require other rules if the test pressure is greater than 2 MPa. | | | | | | | | |
| Answer from the MHD (to be filled by MHD): | | | | | | | | |
| The proposed answ | ver 2 is accepted. | | | | | | | |
| To be sent to EN 1 secretariat: | 3445 Maintenand | ce Help Desk | EN Sta F 9 e-r | l 13445 M andardizat 92038 Pari nail: <u>en13</u> 4 | HD secretariat c/o UNM ion Office on behalf of AFNOR is La Défense Cedex – France 445@unm.fr | | | |



| Request reference number (to be filled by MHD): (2014)-03-64 Date: 201X-xx-xx | | | | | | | | | |
|--|-------------------|---------------------|--------|-------------|--|--|--|--|--|
| Please fulfil the | following | | | | | | | | |
| Part: EN 13445-3 V4 | lssue: 2014 | Page 28 | Sub | clause - | National Standard Reference English | | | | |
| <u>Subject</u> : | Subject: | | | | | | | | |
| Type of request: | 🛛 Tech | nical clarification | on | | Editorial correction | | | | |
| | 🗌 Tech | nical comment | : | | Translation correction | | | | |
| From : | | | | | | | | | |
| Company: Cetim | | | | e-mail: p | hilippe.rohart@cetim.fr | | | | |
| Name: Philippe RO | HART | | | phone: + | 33 3 44 67 47 94 | | | | |
| Postal address: Ave | enue Felix Louat, | Senlis, FRANC | E | | | | | | |
| | 1 | | | | | | | | |
| Manufacturer | 🛛 User | 🗌 Other (p | please | specify): | | | | | |
| | | | | | | | | | |
| Question/commen | <u>it</u> : | | | | | | | | |
| Table 6-1 provides the maximum allowed values of the nominal design stress for pressure parts other than bolts. There are several categories, mainly depending on the question "Is my steel austenitic ?" My question deals with austenitic-ferritic steels. I am hesitating between two interpretations : My austenitic-ferritic is both austenitic and ferritic. So it is austenitic, and should be classified in categories 6.4 or 6.5 My austenitic-ferritic is neither austenitic nor ferritic. So it is not austenitic, and should be classified in categories 6.2 or 6.3 | | | | | | | | | |
| Proposed answer(s | <u>)</u> : * | | | | | | | | |
| Answer 1 : Austenitic-ferritic steels are no austenitic steels. They should therefore be classified in categories 6.2 or 6.3. A note may be added to this table, so as to impose this interpretation. | | | | | | | | | |
| Answer from the MHD (to be filled by MHD): | | | | | | | | | |
| The proposed answer is accepted. | | | | | | | | | |
| To be sent to EN 13445 Maintenance Help Desk secretariat: EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr | | | | | | | | | |



| Request reference | number (to be fille | ed by MHD): (| (2014)- | 05-29 et (| 2014)-03-65 | Date: 2022-05-05 |
|---|--|----------------------|----------------|-------------------------|--|------------------------|
| Please fulfil the f | ollowing | | | | | |
| Part: EN 13445-5 EN 13445-3 | Issue: 2014 2014 | Page 10 477 | Sub 5 18 | clause .2.2 .2.17 | auseNational Standard Reference.2DIN EN 13445-5:2018-12.17DIN EN 13445-3:2016-12 | |
| Subject: critical are | eas / Information to | be contained | in the | technical | documentation | |
| Type of request: | 🛛 Tech | nical clarificat | ion | [| Editorial corre | ction |
| | Tec | nnical comme | ent | | Translation c | orrection |
| From : | | | | | | |
| Company: | Sulzer | Pompes Fran | се | e-mail: | yar | nnick.lecoq@sulzer.com |
| Name: | ······ | Yannick Le Co | po | phone: + | | +33 1 34 77 70 58 |
| Postal address: 1 R | ue de l'Innovation | 78200 Buchela | ay | phone: + | | +33 6 88 97 68 14 |
| Manufacturer | acturer 🛛 User 🗌 Other (please specify): | | | | | |
| Question/commen | <u>t</u> : | | | | | |
| According to EN 13445-5:2014 § 5.2 "Information to be contained in the technical documentation" : "if the vessel is designed for cyclic operation the allowed numbers of cycles, the range of action (as defined in EN 13445-3:2014, 5.3.1) during the cycle and the locations where the cumulative fatigue damage index D (as defined in EN 13445-3:2014, Clauses 17 and 18) is greater than 0.8." technical documentation shall indicate areas where D > 0.8 EN 13445-3:2014 18.2.17 critical area : an area where the total fatigue damage index exceeds the maximum value D _{max} defined as follows: • D _{max} = 0,8 for 500 < n _{eq} <1 000 • D _{max} = 0,5 for 1000 < n _{eq} <10 000 • D _{max} = 0,3 for neq > 10 000 Specific NDT requirements shall apply for critical areas (see 18.4.4). Several thresholds are considered for critical areas according to EN 13445-3:2014 and EN 13445-3:2014 do not look fully consistent. Proposed answer(s): * | | | | | | |
| that EN 13445-5:2014 § 5.2 should be modified accordingly. | | | | | | |
| Answer from the MHD (to be filled by MHD): | | | | | | |
| The proposed answer is acceptable | | | | | | |
| To be sent to EN 13445 Maintenance Help Desk secretariat: EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr | | | | | o UNM alf of AFNOR dex – France | |

* Please note that question with proposed answers will be dealt with as priority.

SULZER CONFIDENTIAL



| Request reference number (to be filled by MHD): (2021)-03-02 Date: 2022-05-05 | | | | | | | | | |
|---|--|---|--------------------|-----------------------------|---------------------------------|--|--|--|--|
| Please fulfil the following | | | | | | | | | |
| Part: EN 13445-3 | lssue: 2021 | Page 363 & 374 | Sub 16.4 16. | clause 1.6.4 & .5.6.4 | National Standard Reference | | | | |
| <u>Subject</u> : | <u>Subject</u> : | | | | | | | | |
| Type of request: | Tech | nical clarificati | ion | | Editorial correction | | | | |
| | 🗌 Tech | inical commen | t | | Translation correction | | | | |
| <u>From</u> : | | | | | | | | | |
| Company:P3 Engin | eering | | | e-mail:W | /.Stikvoort@P3Engineering.nl | | | | |
| Name:Walther Stik | voort | | | phone: + | ·31592347088 | | | | |
| Postal address:Rotterdamseweg 183C - 2629 HD Delft The Netherlands | | | | | | | | | |
| Manufacturer | Manufacturer User Other (please specify): Consultant | | | | | | | | |
| Question/commer | | | | | | | | | |
| Re:Clause 16.4 Add the foll | 4.6.4 of EN 13 owing expressi | 445-3 ons under ec | quation | 1 (16. 4 [.] | -15) | | | | |
| $\sqrt{[(\Phi_{\rm P} + \Phi_{\rm Z})]}$ | [)² + Φ _B]² + | - Ф_T ² ≤ 1.0 | | (| 16. 4-15a) | | | | |
| $\sqrt{\Phi_z^2 + \Phi_B^2}$ | $+ \Phi_T^2 \le 1.0$ | | | (| 16. 4-15b) | | | | |
| $\sqrt{(\Phi_{\rm P} - 0.2)}$ | $ \Phi_{\rm Z} \rangle^2 + \Phi_{\rm B} ^2$ | +Φ ₅ ² ≤ 1. | .0 | (16. 4-15c) | | | | | |
| Re:Clause 1 Add the foll | 16.5.6.4 of EN owing expressi | 13445-3 ons under ec | quation | n (16. 5-1 | 5) | | | | |
| $\sqrt{\left[\left(\left \frac{\Phi_{P}}{c_{4}}+\Phi_{Z}\right.\right]\right)}$ | $)^{2} + \Phi_{B} ^{2} -$ | $\left \Phi_{T}^{2} \leq 1.0 \right $ | | (| 16. 5-15a) | | | | |
| $\sqrt{\Phi_{\rm Z}^{2} + \Phi_{\rm B}^{2} + \Phi_{\rm T}^{2}} \le 1.0 \tag{16. 5-15b}$ | | | | | 16. 5-15b) | | | | |
| $\sqrt{\left(\left \frac{\Phi_P}{c_4} - 0.2 \right \right)}$ | $\sqrt{\left(\left \frac{\Phi_{\rm P}}{c_4} - 0.2 \Phi_{\rm Z}\right \right)^2 + \Phi_{\rm B}^2 + \Phi_{\rm S}^2} \le 1.0 \qquad (16.5-15c)$ | | | | | | | | |
| Proposed answer(s | i): * | interpretation | of the e | equations (| 164.15 and (165.15) | | | | |



Answer from the MHD (to be filled by MHD):

We think that the formulae contained in the standard are clear enough. The proposed answer is not acceptable.

| To be sent to EN 13445 Maintenance Help Desk secretariat: | EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: <u>en13445@unm.fr</u> |
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EN 13445 "Unfired pressure vessels" Maintenance Help Desk (MHD) Question form

| Request reference number (to be filled by MHD): (2021)-03-03Date: 2022-05-05 | | | | | | | |
|--|---|---------------|-------------------------|---|---------------------------------|--|--|
| Please fulfil the | following | | | | | | |
| Part: EN 13445-3 | lssue: 2021 | Page | Clai "Fla | use 11 anges" | National Standard Reference | | |
| Subject: | | | | | | | |
| Type of request: | Type of request: | | | | | | |
| | _ Τε | echnical comm | ent | | Translation correction | | |
| From : Company:P3 Engineering e-mail:W.Stikvoort@P3Engineering.nl Name:Walther Stikvoort phone: +31592347088 Postal address:Rotterdamseweg 183C - 2629 HD Delft phone: +31592347088 | | | | | | | |
| Manufacturer | User Other (please specify): Consultant | | | | | | |
| Question/comment: It has been noted that clause 11 of EN 13445-3 does not include hub slope restrictions as in ASME VIII- 1;Appendix 2 - Figure 2-4 and in ASME VIII-2-Figure 4.16.2. What is the justification for the absence of such manufacturing recommendations 2 | | | | | | | |
| Proposed answer(s): * The appropriate figures showing hub slope restrictions will be incorporated in the next revision of clause 11. | | | | | | | |
| Answer from the MHD (to be filled by MHD): Slope resctrictions are already contained in Annex A. | | | | | | | |
| To be sent to EN 13445 Maintenance Help Desk secretariat: | | | EN Sta F 9 e-1 | EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: <u>en13445@unm.fr</u> | | | |



| Request reference number (to be filled by MHD): (2021)-03-04 Date: 2022-05-05 | | | | | | | |
|---|---------------------|-----------------|--|--|-----------------------------|--|--|
| Please fulfil the | following | | | | | | |
| Part: EN 13445-3 | lssue: 2021 | Page 344-345 | Page Sub- 344-345 15 | | National Standard Reference | | |
| Subject: | Subject: | | | | | | |
| Type of request: | ype of request: | | | | Editorial correction | | |
| | X Technical comment | | | | Translation correction | | |
| From : | | | | | | | |
| Company: Titan Pro | ojects bv | | | e-mail: rs | sp@titanprojects.nl | | |
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| Postal address: De | Marne 53, 8701 F | V Bolsward | | | | | |
| | | | | | | | |
| X Manufacturer | User | Other (p | blease | se specify): | | | |
| | | | | | | | |
| Question/commen | <u>nt</u> : | | | | | | |
| The bending stresses formulas 15.5.3-4, 15.5.3-5, 15.5.3-6, 15.5.3-7, 15.5.3-8 and 15.5.3-9 gives as result the unit N/mm^3 instead of N/mm^2 | | | | | | | |
| Example formular15.5.3-4: (sb)c=((P*e1*h^2)/(8*N*H*I1))*((K2-k1*k2)+a^2*k2*(K2-k2)) result x*N/mm^3 | | | | | | | |
| Proposed answer(s): * | | | | | | | |
| I think this formular should be: (sb)c=((P*e1*h^2)/(8*N*I1))*((K2-k1*k2)+a^2*k2*(K2-k2)) result x*N/mm^2 | | | | | | | |
| For the other formulas the same change. Leaf the length H out of the formulas | | | | | | | |
| Answer from the MHD (to be filled by MHD): | | | | | | | |
| CEN/TC 54/WG 53 agrees that the formulae are wrong. For a solution, see the answer to the question (2021)-03- 05. | | | | | | | |
| To be sent to EN 13445 Maintenance Help Desk Si Secretariat: | | | | EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr | | | |



| Request reference number (to be filled by MHD): (2014)-04-05 Date: 2019-12-23 | | | | | | |
|---|---|---------------|----------------------|---------------------------------------|---|--|
| Please fulfil the following | | | | | | |
| Part: EN 13445-4 | lssue: 3 | Page 20 | Page Subcl 20 7.3 | | National Standard Reference SS-EN 13445-4:2014 | |
| Subject: | | | | | | |
| Type of request: | Type of request: Image: Technical clarification Image: Decision Total clarification Technical clarification Technical clarification | | | | Editorial correction | |
| | | nical comment | | | Translation correction | |
| From :Company: Kiwa Inspecta ABName: Karin VelanderPostal address: P.O.Box 7178, 170 07 Solna | | | | arin.velander@kiwa.com 46104793509 | | |
| Manufacturer | r 🗌 User 🛛 Other (please specify): Notified Body | | | | | |
| Question/comment:EN 13445-4 clause 7.3 a) state that:For test plates on butt joints equal to or over 20 mm thickness a longitudinal weld tensile test having a minimum diameter equal to or over 6 mm shall be performed in accordance with EN ISO 5178:2011 and R_{eT} , R_m and A_5 shall satisfy the specified minimum requirements of the base material or for weld consumables requirements in EN 13445-2:2014, 4.3.5 or other relevant values specifically taken into account in the design (e.g. austenitic filler metal in combination with 9 % Nickel steel).Where the design temperature is higher than 300 °C then the test shall be done at the design temperature.Question:Shall the long weld tensile test be performed at design temperature only when the design temperature is higher than 300 °C?Proposed answer(s): *No, it shall satisfy the specified minimum requirements of R_{eT} and this value is the yield strength at the calculation temperature T, though the test shall be performed at the calculation temperature. | | | | | | |
| Answer from the MHD (to be filled by MHD): | | | | | | |
| This draft amendment EN 13445-4:2021/FprA1 under completion answers this MHD question. | | | | | | |
| To be sent to EN 1 secretariat: | To be sent to EN 13445 Maintenance Help Desk secretariat: EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr | | | | | |



Question form

| Request reference number (to be filled by MHD): (2014)-04-07 Date: 2021-02-03 | | | | | | | | |
|--|-------------------------------|--------------------|-----------------------------------|---------------|---|--|--|--|
| Please fulfil the following | | | | | | | | |
| Part: EN 13445-4 | Issue: 2014-V4-2017- 07 | Page 65 | Subclause Annex C § C.5.5.1 | | National Standard Reference NF EN 13445-4 V4 | | | |
| Subject: | | | | | | | | |
| Type of request: | ⊠ Tech | nical clarificatio | n | Editorial | correction | | | |
| From . | | nical comment | | I ranslatio | on correction | | | |
| Prom. Company: APAVE e-mail: charles.jarboui@apave.com Name: Charles JARBOUI phone: +33 6 66 95 61 38 Postal address: Immeuble Canopy – 6 Rue du Général phone: +33 6 66 95 61 38 Audran - CS 60123 92 412 COURBEVOIE Cedex FRANCE FRANCE | | | | | | | | |
| Manufacturer | User | Other (p | lease specify) | : Notified Bo | ody | | | |
| Question/comment: The majority of the qualification standards for permanent joining personnel specify that the date of starting of validity period of the qualification must be based on the date of production of the qualification coupon. Against this common general provision, EN 13445-4 Annex C § C.5.5.1 specifies that the validity of the approval of an expanding operator starts from the moment when all the required tests have been carried out and approved. Can you please take the necessary steps to bring this specific feature up and correct it in Annex C of EN 13445-4 to make it consistent with the rule of all other qualification standards for personnel in charge of permanent joining? Or produce an interpretation for this item accordingly. Indeed, this peculiarity creates difficulties in the processing and management of the qualifications of expanders according to this Annex C. EN 13445-4 Annex C § C.5.5.1: "C.5.5 Period of validity C.5.5 Period of validity Proposed answer(s): * We propose to use the same wording as provided by the harmonised standard EN ISO 9606-1 for the qualification of welders (see below). Example of EN ISO 9606-1: "9 Period of validity 9.1 Initial qualification | | | | | | | | |
| Answer from the MHD (to be filled by MHD): | | | | | | | | |
| This technical issue to be considered. Clarification of the text is necessary. The proposed changes of this MHD question should be included into the Draft Amendment under development EN 13445-4:2021/prA2. | | | | | | | | |
| To be sent to EN 13445 Maintenance Help Desk secretariat:EN 13445 MHD secretariat c/o UNM Standardization Office on behalf of AFNOR F 92038 Paris La Défense Cedex – France e-mail: en13445@unm.fr | | | | | | | | |